

AG 52 FSW

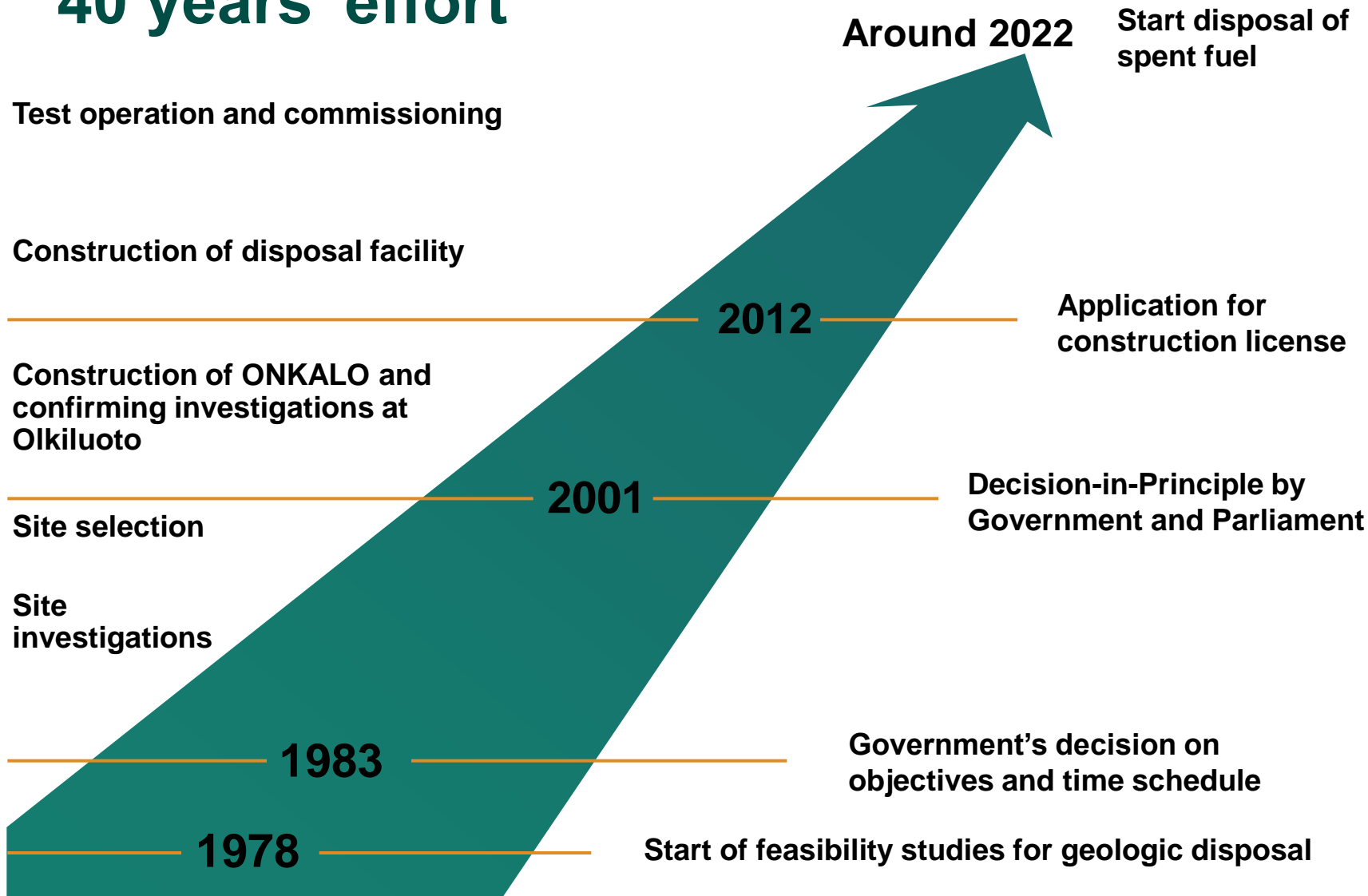
Posiva's welding method
selection for sealing copper
canister



Presentation

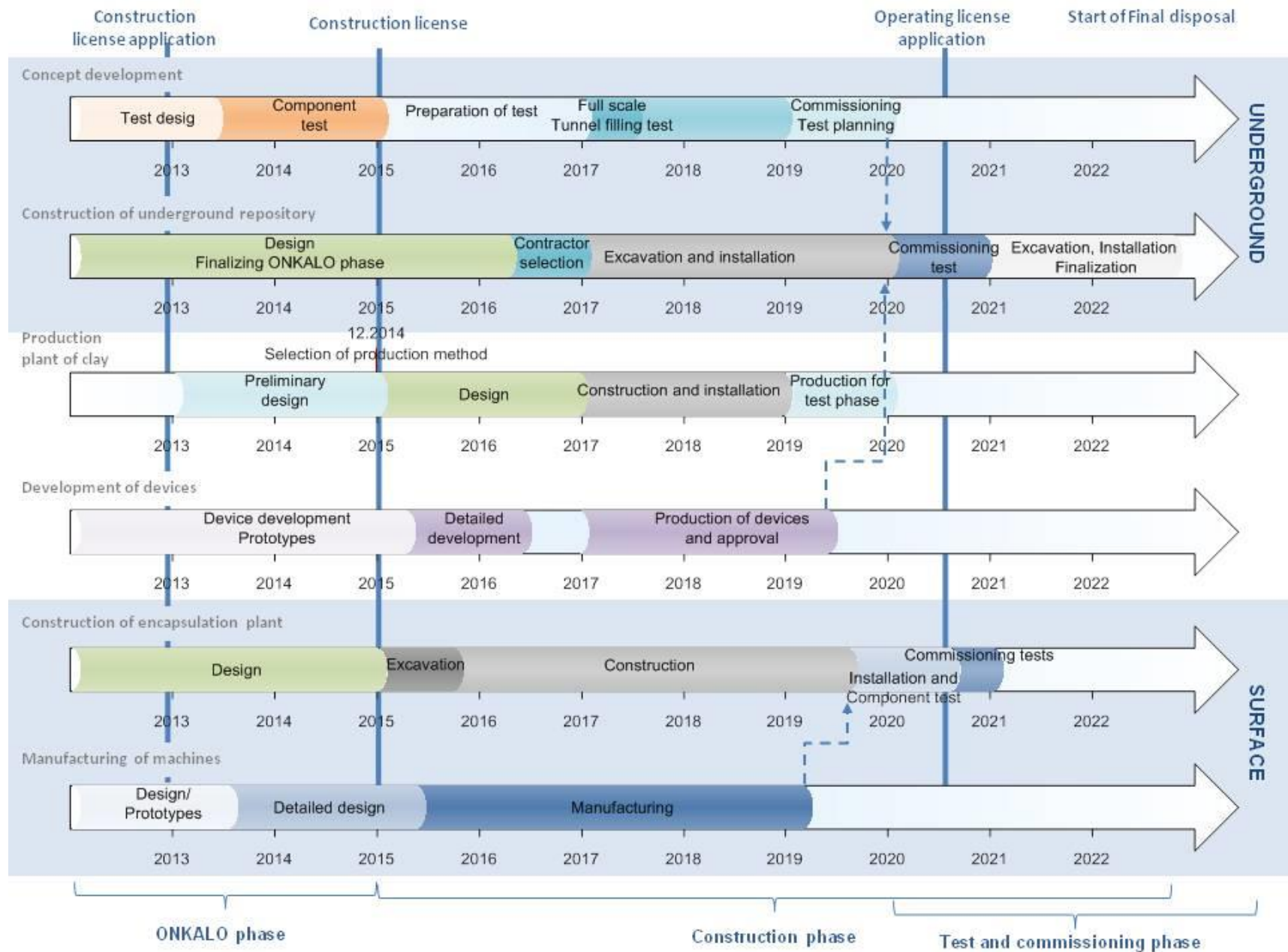
- Overall information about Posiva's timetable concerning starting final disposal and concept
- Basics of the Posiva's choosing process of the welding method for sealing copper canister
- Demands for the canister weld set by VAHA
- Welding tests during year 2013 with SKB

40 years' effort



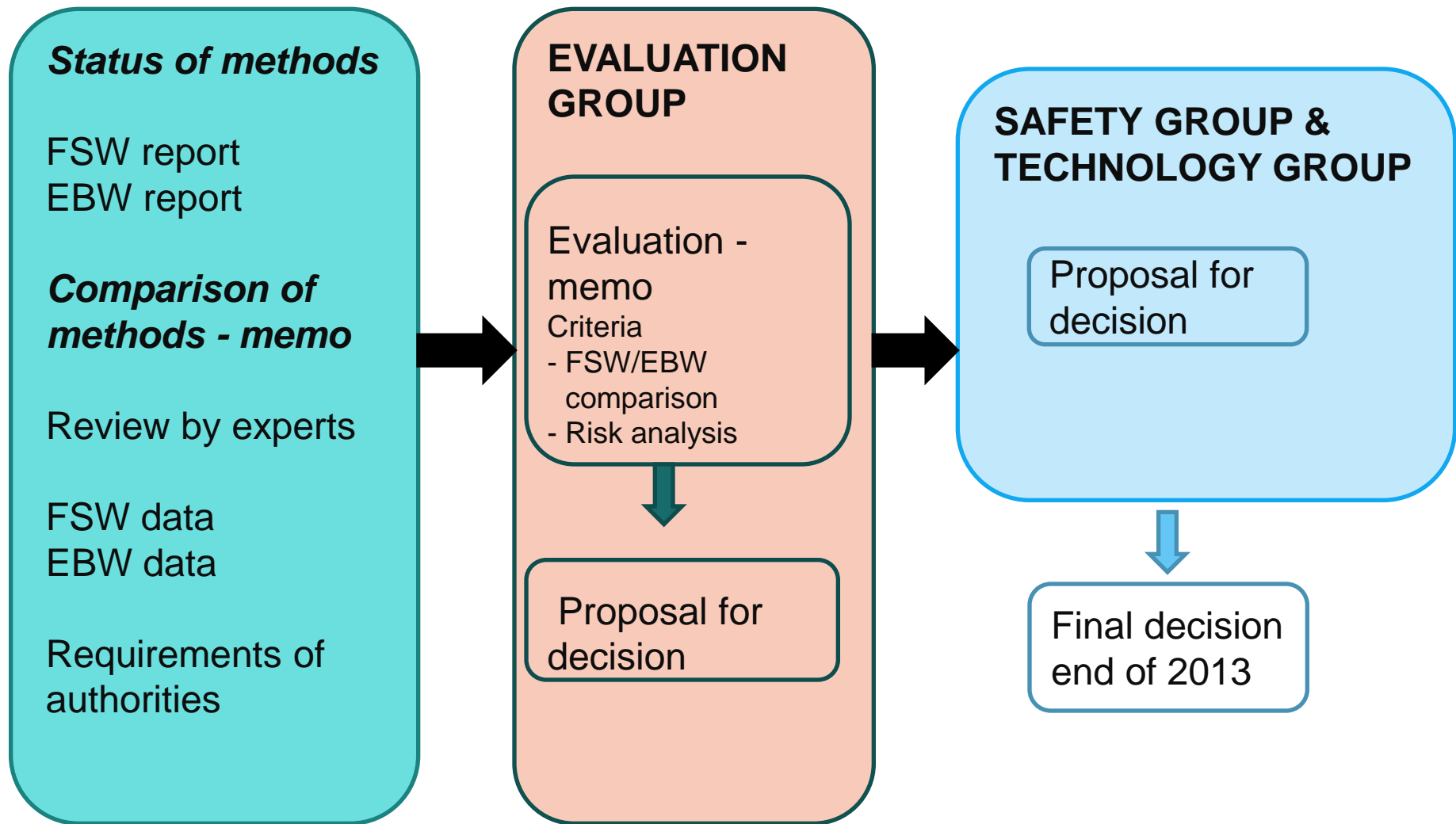
Status of the Application

- Posiva submitted 29.12.2012 the construction license application for TEM's (ministry) review
 - application and associated (18) app's
 - TEM requested statement's from ~ 20 organisations
 - STUK has promised to give it's statement within about 18 months
 - application has been translated in Swedish
- Construction license is expected to be granted within about 2 years

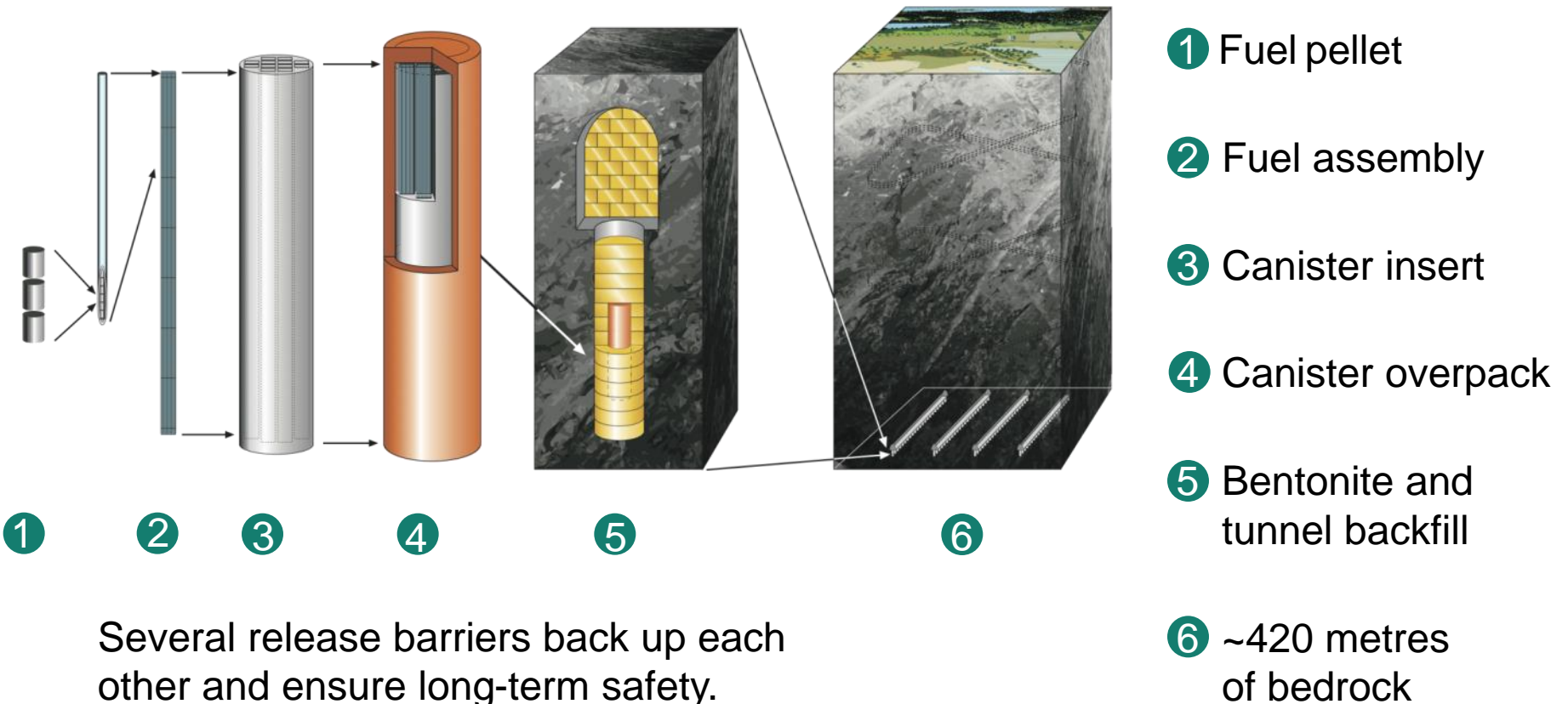


Background of the choosing process

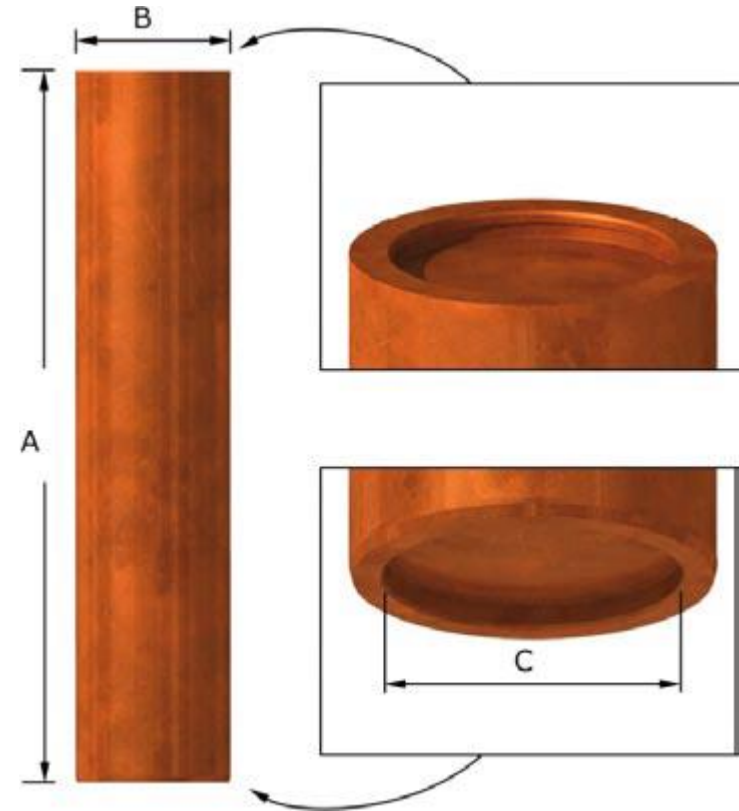
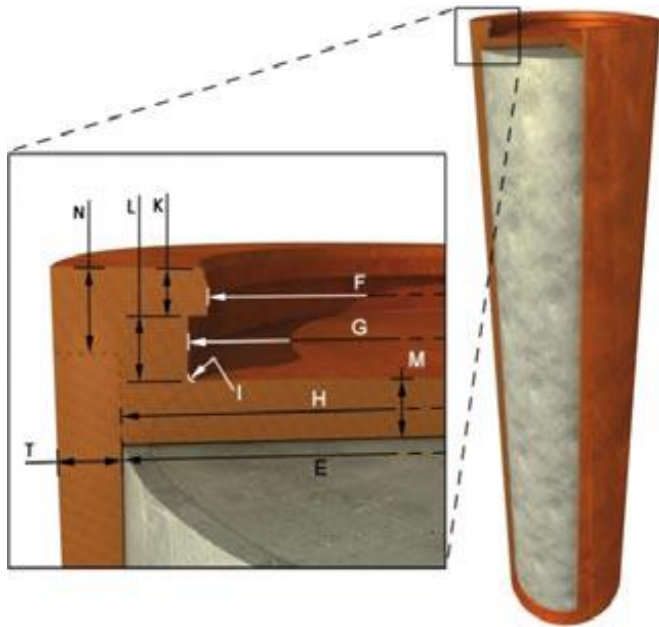
- SKB chose the reference welding method during years 2005 – 2006. Selection was done between FSW and EBW.
- Posiva will choose the welding method at the end of year 2013. Selection will be made between FSW and EBW



The principle of final disposal (KBS-3V)



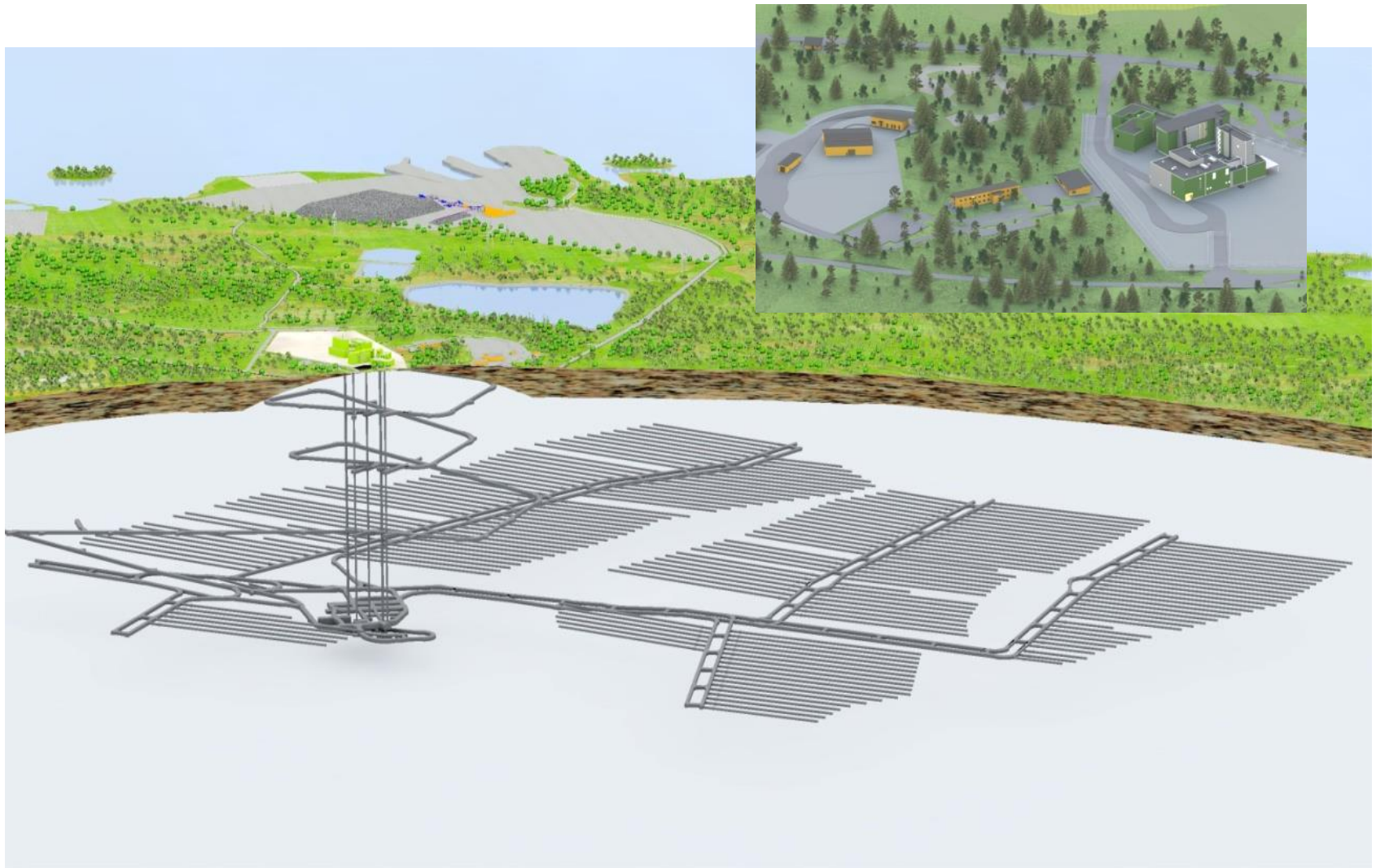
Dimensions of the canister



A = 3552 – 5223 mm
B = 1050 mm

mass of the copper = 5.6 – 8 ton
total canister mass = 18.8 – 29 ton

Final repository around 2120's (9000 tU)



VAHA - Posiva's requirement management system.

Requirements for the initial state and the long-term safety of the canister welds

- nominal thickness of the overpack is 49 mm
- minimum intact copper thickness is 35 mm and 40 mm in 99% of the canisters' wall thicknesses
- components shall not have macroscopic defects larger than 15 mm in depth
- chemical composition shall fulfil the specification in EN 1976:1998 with the following additional requirements: $O < 5$ ppm, $P = 30 - 100$ ppm, $H < 0.6$ ppm, $S < 8$ ppm
- elongation at rupture shall be $> 40\%$
- creep ductility of the overpack shall be $> 15\%$

VAHA - Posiva's requirement management system.

Requirements set by NDT, manufacturing and handling in encapsulation and disposal plant

- Capacity of the welding process has to be 40 to 60 canisters per year.
- Maximum grain size of the weld and base material has been set to 360 μm to enable sufficient material properties concerning ultrasonic
- Because of high radiation level near canister, system has to be remote controlled.
- Welding system has to produce a weld, which fulfils the acceptance criterions. Reliability of the welding system has to be good and yield of the production has to be high enough to minimize quality costs

Chemical composition of weld material

Chemical composition of the weld material should be such that creep ductility and corrosion properties don't impact long term safety of the copper canister.

	P, [ppm]	S, [ppm]	H, [ppm]	O, [ppm]
VAHA	30 - 70	< 8	< 0.6	< 5
Base material	44 – 52	4 - 5	0.2 – 0,5	1 - 2
FSW weld material	48 - 56	< 5	0,2 – 0,4	2
EBW weld material	50 - 52	4.9 - 5.2	0.2 – 0.4	1.5 – 2.7

Mechanical properties – FSW vs EBW

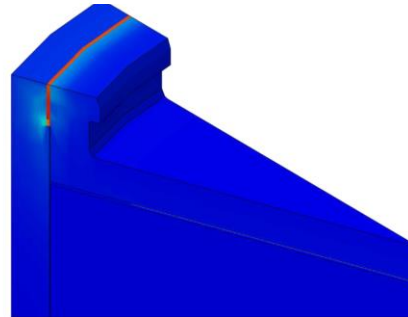
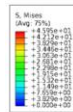
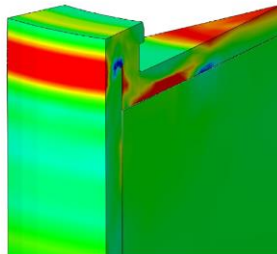
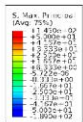
		Temp. [° C]	Rp0.2, [MPa]	Rm, [MPa]	A, [%]
Demand set by VAHA					> 40
EBW	Base material	20	49	201	58
	Weld, transversal	20	48	193	34
	Weld, longitudinal	20	41	188	50
FSW	Base material	20	76	206	51
	Weld	20	75	207	51
	Weld	100	69	198	45

Creep properties – FSW vs. EBW

VAHA: Creep ductility of the overpack shall be > 15% at 80 - 90 ° C

FSW:

Location of the tests specimen	T [°C]	Stress [MPa]	Elongation [%]	Red. of area [%]	Time [h]
base material	175	145	38.9	85.7	163
cross-weld top	175	150	38.3	87.5	40
cross-weld bottom	175	147	35	85.6	45
cross-weld radial, test 1	175	136	13.5	48	7.8
cross-weld radial, test 2	175	136	10	41	11,2
cross-weld radial, test 3	175	126	16	75	14,9



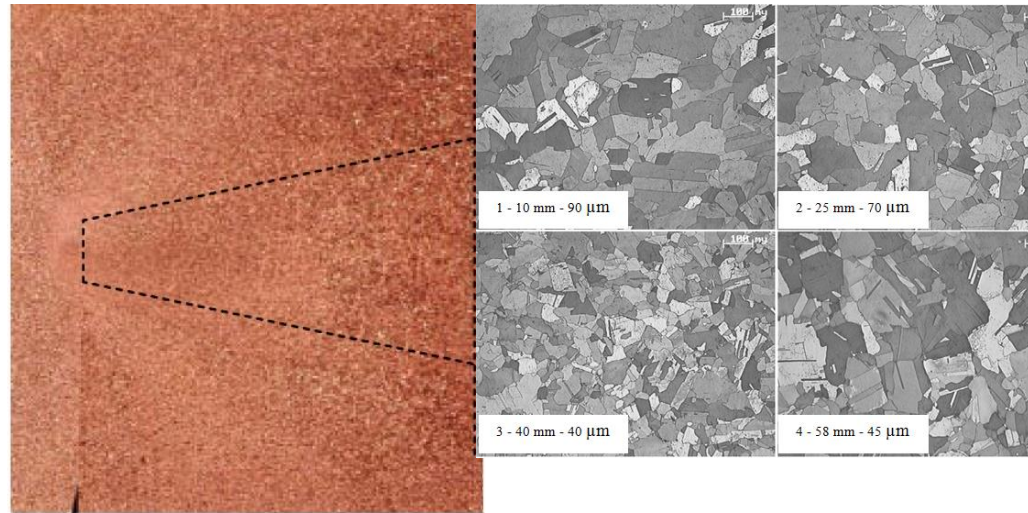
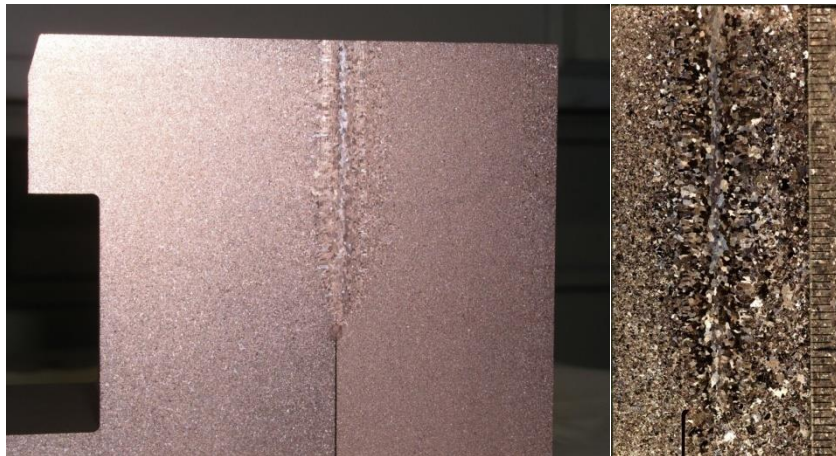
EBW:

Specimen ident	Temperature T (°C)	Nominal stress σ (MPa)	Time (h)	Engineering strain ϵ_f (%)	Area reduction Z (%)	True stress σ_{true} (MPa)	True strain ϵ_{true} (%)
8J	175	125	194	23	67	379	111
9J	175	120	471	25	59	305	89
9N	175	115	844	20	55	256	80
8N	175	100	4405	15	52	208	73
8I	175	100	4656	16	44	179	58
8C	225	95	210	10	34	144	42

FEM-modelling of the initial state

Grain size – FSW vs. EBW

- EB-welds grain size at transversal direction is 0.5-1.5 mm and at longitudinal 10 – 15 mm.
- Average grain size at FS weld is 75 μm .

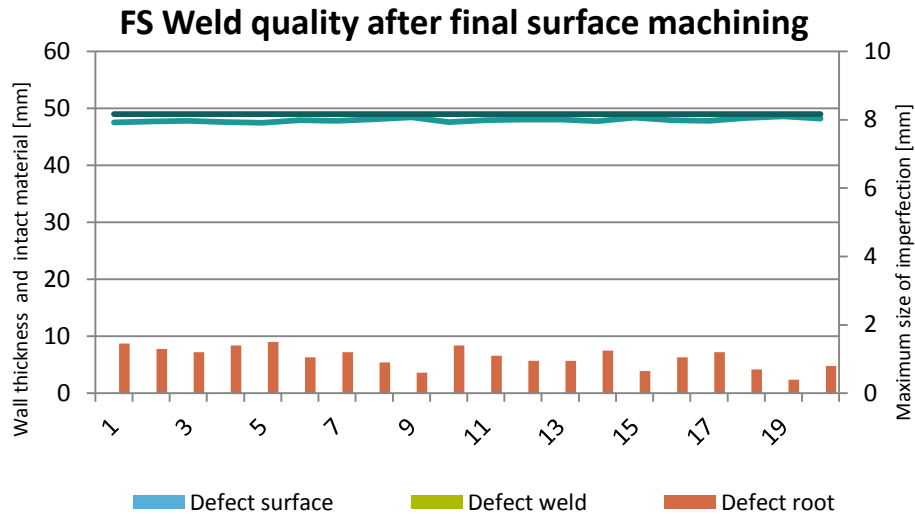


Corrosion

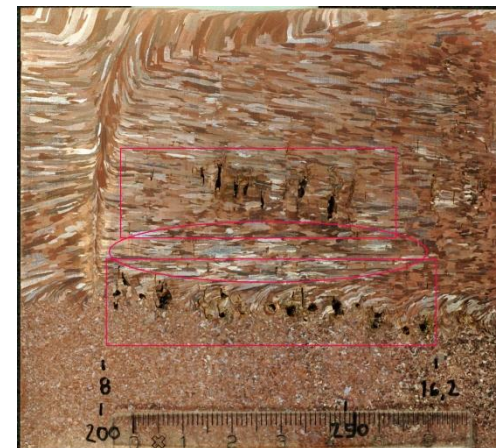
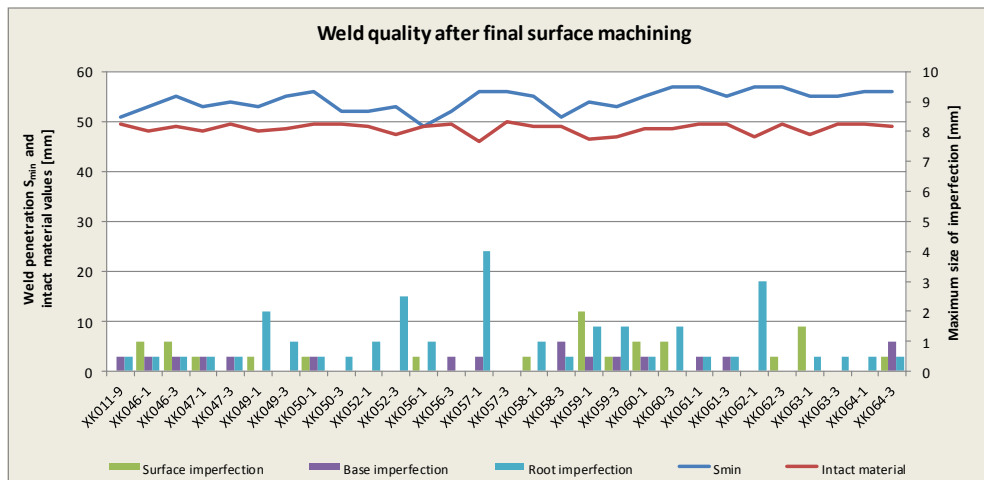
- Possible types of corrosion at final disposal environment:
 - Grain boundary corrosion -> impurities at weld material and grain size
 - Stress corrosion -> residual stresses
 - Galvanic corrosion -> possible impurities at weld material
 - Overall corrosion
- The conclusion from made studies is that there is no evidence to indicate that the weld region should suffer higher corrosion rates than the rest of the canister shell
- Of the two techniques, it can be said that FSW provides better corrosion resistance than EBW welds, because of the lower residual stresses, the minimal grain growth and the absence of any resultant concentration of impurities at the grain boundaries

for FSW

Intact material



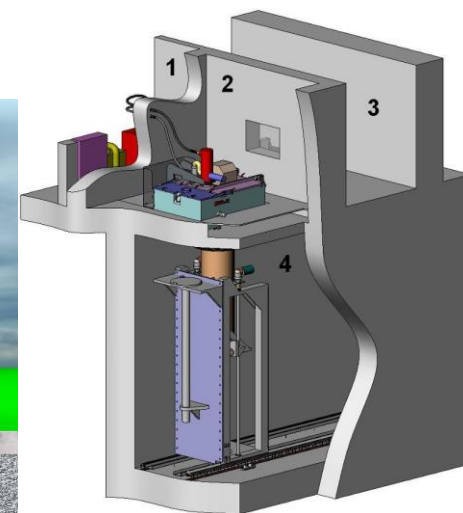
JLH



Cold shut

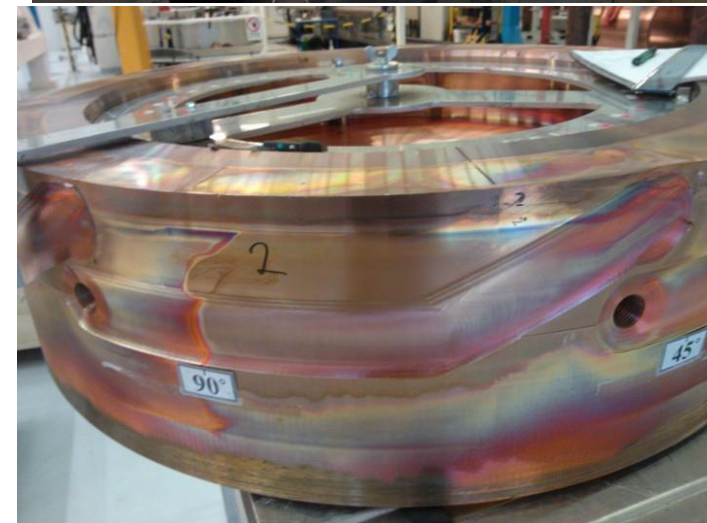
Implementation of the welding machine to the encapsulation plant

- There has been made comprehensive plans for implementation of the EBW-machine at encapsulation plant
- Basics concept of the welding operations is similar



FSW 2013 – welding tests of 5 lids

- During spring 2013 Posiva and SKB welded 5 lids at Oskarshamn.
- 3 tests lids were supposed to use for research that how much does manufacturing method of the components and S-content affects to welding
- lid nro. 4 is used to improve knowledge of Posiva's NDT-work for inspection of the FS-welds



Kiitos
Thank you

